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(54) Fibrin gel containing catalytic active substances.

(57) A fibrin gel containing therein means for retaining the
shape against deformation and at least one catalytical active
substance.

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BACKGROUND OF THE INVENTIONField of the Invention

This invention relates to a filter with a definite pore size comprising fibrin and a process for the preparation thereof from fibrinogen. This invention also relates to a size selective process employing the filters of the invention.

DISCUSSION OF PRIOR ART

Formation of fibrin gels by contacting fibrinogen with a coagulation enzyme has long been known. According to quotation no. 55888k in "Chemical Abstracts" Vol. 84, No. 9, 1.3.76, it is known to embed chloroplast ATPase (CF_1) in fibrin membrane, which is formed by fibrinogen-fibrin conversion in the presence of thrombin and is stabilized by blood-coagulation factor XIII under physiological conditions. This immobilized chloroplast ATPase has the potent ATPase activity, 0,3 umoles phosphate/mm²/min and does not cause the cold inactivation of the enzymic activity.

Furthermore quotation no. 126372h in Chem. Abstr. Vol. 88, No. 17, 24.4.78 reports of fibrin membranes being used for immobilization of enzymes (such as asparaginase) to stabilize the enzymes. Fibrinogen solutions are treated with thrombin at 30 to 40°C. Thin clot membranes are formed in the presence of calcium. The membranes are dried to a water content of less than 20%.

It has been observed that when a liquid is passed over the gel, permeation of the gel increasingly becomes difficult - sometimes to the point where permeation and passage of the liquid are rapidly diminished or cease. It was believed that the gel infrastructure was extremely

1 fragile and that the gel consisted of networks of channels
and pores of varying size which were highly changeable, and
highly dependent upon and variable with liquid or liquid
5 mixtures passed thereover, especially one having solid
particles.

It was therefore thought that such fibrin gel
was not useful in separating components where the
separation was effected solely on the basis of particle
10 size.

Specifically, when investigating the fibrin
formation from fibrinogen the interest was directed to the
flow properties of fibrin gels. It has e.g. been shown
15 before that the flow properties through silica gel as well
as through agar and gelatin gels are such as for a viscous
flow. It has also been shown earlier that the flow through
a fibrin gel is dependent upon the ionic strength and
fibrinogen concentration

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in the preparation. In the investigations made, the permeability coefficient (K_s) of the fibrin gels was determined by Poiseuille's law as follows: (Darcy coefficient) $K_s = \frac{Q \cdot L \cdot n}{t \cdot A \cdot \Delta p}$ (1)

wherein Q is the flow through the gel in cm^3 , A is the gel surface in cm^2 , Δp is the pressure difference in dynes/ cm^2 ($=0.1 \text{ N/m}^2 = 0.1 \text{ Pa}$), t is the time in seconds, L is the length of the gel in cm and n is the viscosity in poise ($=0.1 \text{ Pa} \cdot \text{s}$). Moreover, Kozeny-Carman has shown that the following relationship applies in a viscous or laminar flow in a capillary system:

$$m = \sqrt{\frac{K_0 \cdot K_s}{\cos^2 \phi \cdot \epsilon}} \quad (2)$$

wherein m is the hydraulic radius ($\frac{\text{wetttable surface}}{\text{wetttable circumference}}$).

in cm, K_0 is a factor decided by the geometry of the capillaries, and ϕ is the orientation (angle) of the capillaries to the direction of flow, ϵ is the partial share of liquid in the gel and r is the radius of the capillaries in cm. ϵ can be calculated by means of the protein concentration and with a knowledge of the partial specific volume of the fibrinogen which is 0.72. For gels of the type concerned here K_0 and $\cos \phi$ cannot be calculated. In the theoretical calculations it has been assumed here that the capillaries are cylindrical and parallel to the direction of flow, which according to Madras et al brings the indicated formula to the following:

$$r = 2m = \sqrt{\frac{8 \cdot K_s}{\epsilon}} \quad (3)$$

The theoretical pore size is therefore $2r$. By effective pore size we mean: the size at which particles of smaller size pass through the pores and particles of larger size are retained.

It has appeared from the tests that the clotting time (time of gel

formation) of the thrombin-fibrinogen mixture, h r called Ct , is directly proportional to the flow (Q) through the gel. The flow (Q) has further been found to be inversely proportional to the fibrinogen concentration (C). Provided $Q = 0$, when $\frac{1}{C} = 0$ and $Ct = 0$, the equation (1) will have the following form:

$$K_s = \frac{k \cdot Ct \cdot K \cdot n}{C \cdot A \cdot P \cdot t} \quad (4)$$

wherein k is a constant which is dependent on pH, ionic strength and calcium concentration and, moreover, is characteristic of the enzyme used in the gel formation, and Ct is the clotting time in seconds. The other symbols are the same as in equation (1). The term t is omitted when the flow is expressed in cm^3/s . According to this equation the permeability coefficient K_s is thus directly proportional to the clotting time Ct and inversely proportional to the fibrinogen concentration.

By varying the pH between 6 and 10 the ionic strength between 0.05 and 0.5, the calcium ion concentration between 0 and 20 mM and/or the concentration of enzyme (e.g. thrombin, "Batroxobin" or "Arvin") between 0.01 and 10 NIH-units (or the corresponding units of other enzymes) per ml solution and the fibrinogen concentration from 0.1 and up to 40 g/l, preferably between 1 and 10 g/l, gels with K_s -values [calculated according to the equation (1)] between 10^{-7} and 10^{-12} , preferably between 10^{-8} and 10^{-11} , can be prepared. Calculated according to the equation (3), the corresponding average radii will be 0.03 - 9 μm , preferably 0.09 - 2.8 μm . If FXIII (a transamidation enzyme) and calcium ions are present in the gel formation the stability of the gels will be increased as covalent cross-

1 linkings will arise between the chains in the subunits of the
2 gel matrix.

3
4 Thus, now it has been found according to the inven-
5 tion that these fibrin gels can be used as a filter. The
6 filter according to the invention is characterized in that it
7 is built of fibrin and the fibrin gel is in association with a
8 shape-retaining means which retains the shape of at least one
9 surface of said gel against deformation when contacted by a
10 flowing liquid.

11
12 The filter of the invention has substantially
13 uniform pores. By that is meant that the standard deviation
14 of pore size is less than 15 percent, preferably less than
15 10 percent and in some instances less than 5 percent.

16
17 The pore size of the gel has, moreover, been found
18 to be a function of the clotting parameters used in the gels'
19 preparation, i.e., the pore size is varied by changing said
20 parameters. The pore size is then proportional to the clotting
21 time.

22
23 It has now been discovered, in accordance with the
24 invention, that fibrin in gel form can be used as a filter
25 if means are provided to retain the shape of at least one
26 surface of the gel against deformation when the gel is contacted
27 by a flowing medium such as a flowing liquid medium containing
28 components to be separated. It has also been discovered, quite
29 surprisingly, that the gel has substantially uniform pore sizes
30 and that these pore sizes can be regulated simply by altering
31 the process parameters employed for the formation of the gel

1 Specifically, it has been discovered, if the gel is
2 in some way stabilized by a shape-retaining means, that the
3 gel structure is preserved and the uniform pores therein func-
4 tion ideally as a filter medium.

5
6 Generally speaking, the gel is brought in contact
7 with a shape-retaining means. The shape-retaining means can be
8 a foraminous member such as a foraminous sheet member and is
9 preferably disposed on or in association with an upper surface
10 of the gel, preferably in contact with the gel either directly
11 or through an adhesive or a graft. Since the foraminous mem-
12 ber serves to preserve the shape and structure of the upper
13 surface of the gel when the medium to be filtered contacts the
14 same, the gel does not collapse, thereby allowing the uniform
15 pores thereof to function ideally as a filter medium.

16
17 Foraminous members functioning as shape-retaining
18 means can have virtually any size and shape, although they are
19 preferably in the form of a sheet and preferably are substan-
20 tially co-extensive with the upper surface of the gel. The
21 foraminous sheet members can be in the form of a fibrous net-
22 work such as in the form of a woven or non-woven or knitted
23 fabric, the fibers of which can be natural or synthetic.

24
25 When the fibers of a foraminous sheet member are
26 natural, they can be, for example, made of silk, wool, cotton,
27 cellulose, hemp, jute or the like.

28
29 As synthetic fibers, there are contemplated in
30 particular fibers made of nylon, polyester, polyolefin, fibers

1 made of vinyl polymers, acrylics such as polyacrylonitrile,
2 rayon, to name a few.

3
4 The fibers generally have a thickness between 1 μ m
5 and 1000 μ m, preferably between 10 and 20 μ m, and are disposed
6 in relationship to one another to define openings therebetween
7 of between 0.01 and 5 mm, preferably between 0.05 and 1 mm,
8 it being understood that the size of the openings between the
9 fibers of the foraminous sheet is not especially critical, pro-
10 vided it allows passage therethrough of the medium to be filtered.
11 It is preferred that as much fiber be in contact with or adhere
12 to the gel as possible so as to insure maximum structural in-
13 tegrity of the surface of the gel initially to come in contact
14 with the medium to be filtered.

15
16 Instead of using a fibrous foraminous member, one
17 can use one made of wires, such as wires made of copper, tin,
18 zinc, aluminum, glass, boron, titanium, steel, stainless steel,
19 etc. The wires function analogously to the function performed
20 by the fibers in providing structural integrity to at least
21 one surface of the gel, preferably the upper surface or sur-
22 face which is to be initially brought in contact with a mixture
23 to be filtered. The interstices between the wires are of the
24 same magnitude as the interstices between the fibers of a woven,
25 non-woven or knitted fabric serving as a foraminous sheet
26 member. The wires can be in the form of a screen, wire mesh
27 or an expanded wire sheet and are preferably co-extensive with
28 at least one side of the gel, preferably the upper surface.
29
30

1 The gel has uniform pores but owing to the manner
2 by which the gel can be formed, can have uniform pores over a
3 wide range. Preferably, the substantially uniform pores of
4 the fibrin gel have a theoretical pore size or diameter in the
5 range of about 0.003 to ¹9 μ m, more preferably 0.009 to ^{0,3}2.8 μ m.

6
7 The gel is formed by contacting fibrinogen with
8 an enzyme, especially a coagulation enzyme. Particularly con-
9 templated enzymes for use in forming a fibrin gel include
10 thrombin, Batroxobin, Arvin, Eccarin, Staphylocoagulase,
11 Papain, Trypsin, caterpillar venom enzyme, etc.

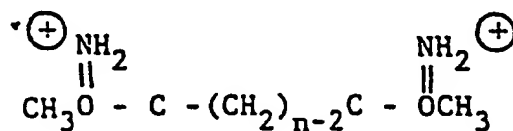
12
13 Generally speaking, the gel formation is effected
14 at room temperature, although temperatures from -3°C up to 58°C
15 can be employed. Preferably, the temperature is in the range
16 of 0° to 40°C.

17
18 It is preferred that the gel be formed by contacting
19 the fibrinogen with an enzyme in the presence of calcium ions.
20 The calcium ion concentration can be up to 20 mM. The presence
21 of calcium ions is not required in all instances. Where
22 thrombin is employed as the coagulation enzyme, the gel can
23 be formed in the absence of a calcium ion.

24
25 In forming the gel, there is generally employed
26 0.1 to 10^{-5} enzyme units per gram fibrinogen, preferably 10 to
27 10^{-3} enzyme units per unit weight fibrinogen. Following forma-
28 tion of the gel whose coagulation time is a function of the
29 relative amount of enzyme to fibrinogen as well as the con-
30 centration of calcium ion, the gel is preferably hardened or

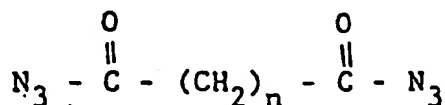
set by crosslinking the components thereof by contacting the gel with a crosslinking agent. Crosslinking agents contemplated include bis-imidates such as suberimide, azides like tartryl di(ϵ -amino caproylazide), aryl dihalides like 4,4-difluoro-3,3'-dinitrophenyl sulfone, glutardialdehyde, nitrenes, N,N'(4-azido-2-nitrophenyl)-cystamine dioxide, cupric di(1,10-phenanthroline), dithio bis-(succinimidyl propionate); N,N'-phenylene dimaleimide as well as polyethyleneimides and other bifunctional compounds, especially those known to crosslink with epsilon lysine, alpha amino groups, carboxy groups of aspartic and glutamic acids, and hydroxyl groups of amino acids in the protein chain (e.g. threonine and serine).

Bis-imidates which can be used include those of the formula



wherein $n = 3$ to 15 especially 3 to 10.

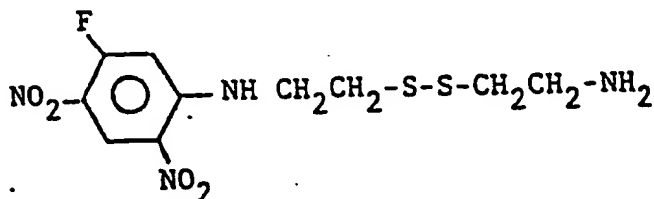
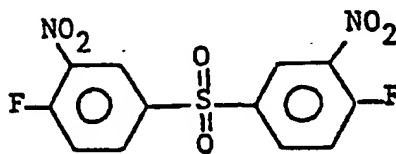
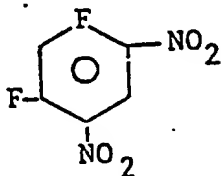
Azides which can be used include substituted and unsubstituted azides of the formula



wherein $n = 1$ to 20 especially 1 to 15. Azides contemplated include those having a hetero atom in the chain, especially nitrogen. Also contemplated are hydroxy substituted azides.

Aryl dihalides which can be used include those having mono, poly and fused rings as well as rings joined by a

direct bond or through a methylene bridge or a sulfo bridge.
 The halogen of the halide can be fluorine, chlorine, or bromine.
 The compounds can be substituted by inert or functional groups
 such as nitro, or disulfide. Contemplated compounds include
 those where a functional group has replaced one of the halo
 substituents, e.g. nitro. Compounds contemplated include



Especially contemplated is glutardialdehyde.

Generally speaking, the crosslinking agent is employed in an amount of between 0.001% and 8 % by weight, preferably between 1 and 2 % by weight of the gel for 1-120 minutes. Crosslinking is effected at temperatures of between 10° and 40°C, preferably 20° to 25°C. After the hardened or crosslinked structure is obtained, the gel is usually washed free of extraneous material.

The gel in such hardened form is useful as a filter, i.e., without any foraminous sheet material. Preferably, however, the gel is formed on or in association with a shape-

1 retaining means such as a net, wire mesh or other sheet material
2 and while in contact with such shape-retaining means is hardened
3 by the use of a hardening or crosslinking agent.
4

5
6 Preferably, the gel is supported on its upper and
7 lower surfaces by a shape-retaining means such as a foraminous
8 sheet or the like, whereby to insure that the gel retains its
9 shape during use as a filter.

10
11 This invention further contemplates a process for
12 separating a first substance having a theoretical size of 0.03
13 to ¹9 μ m from a second substance having a larger size which com-
14 prises passing a mixture of said first and second substances
15 over a filter comprising fibrin in gel form and having pores of
16 substantially uniform size, said filter having means for retain-
17 ing the shape of at least one surface of said gel against de-
18 formation when contacted by a flowing medium, wherein the ef-
19 fective pore size of said fibrin gel is larger than the particle
20 size of said first substance and smaller than the particle size
21 of said second substance. Preferably, the pores of the gel
22 have a theoretical size of 0.009 to 2.8 mm.

23
24 The filters of the invention are important, as they
25 permit the separation of bacteria and viruses from mixtures con-
26 taining the same. The ability to regulate the pore size and
27 to achieve a gel of uniform pore size is an important and criti-
28 cal characteristic of the filters of the invention. These filt-
29 ers permit the separation of blood components, the separation of
30 components of blood plasma, the removal of platelets from blood,
31 the fractionation of cells and cell fragments and the separa-
32 tion of high molecular weight protein aggregates. In addition,

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a variety of particles such as latex, silica, carbon and metallic particles may be separated over these filters. Components which can be separated include those shown in the table below:

TABLE A

Material A Separated	Material from Which Material "A" is Separated	How Separated		Effective Pore Size Range for Filter
		Retained	Eluted	
Blood platelets	Blood plasma	X		Below 1 μ m
Red blood cells	" "	X		1 μ m and below
Sendai virus	Culture medium	X		0.1 μ m and below
" "	" "		X	0.2 μ m and above
Liver mitochondria	Cyto plasma	X		0.5 μ m and below
" "	" "		X	0.5 μ m and above
Adeno virus	Culture medium	X		0.05 μ m and below
" "	" "		X	0.1 μ m and above
E. coli bacteria	" "	X		1 μ m and below
FVIII complex	High molecular weight material (h.m.w) separated from low molecular weight material (l.m.w)	X (h.m.w)	X (l.m.w)	0.05 μ m and below
Blood leucocytes	Blood plasma	X		1 μ m and below
Blood lymphocytes	" "	X		1 μ m and below

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Fibrin gel filters have above all the advantages over other gel filters that the pore size can be simply varied as desired. Moreover, the present filters have high flow rates at such pore sizes as can be used to remove very small particles, such as virus particles. In this respect, the filters of the invention are more suitable than known membrane filters and filters of polyacrylamide gels. The absence of absorption of protein on the filters is also an advantage as compared with certain other filters.

DESCRIPTION OF SPECIFIC EMBODIMENTS

The process according to the invention for the preparation of gel filters is as described above, characterized in that a fibrinogen solution with preadjusting clotting parameters is mixed with a coagulation enzyme and the resulting mixture is made to clot in a form intended for the filter. It may be convenient to strengthen the fibrin gel formed during or after clotting by a shape-retaining means of greater strength than the gel which is preferably applied to the upper surface of the gel to be prepared and preferably to both the upper and lower surfaces thereof.

The shape-retaining means (reinforcing meshes) are preferably in the form of a net which is applied at the lower and preferably also at the upper surface in the mold in which the fibrinogen mixture is poured (cast). This mixture can preferably penetrate the net (foraminous sheet material) e.g. have its surface 10 μ m-5mm, preferably 0.5-2 mm, from the net. The net can have a mesh width, for example, 10 μ m to 5 mm, preferably 50 μ m-1mm and the wire diameter can be, for example, 0.01-1.0 mm preferably 0.1-0.5 mm, where wires are employed as a shape-retaining means. In addition to the metallic wires noted

1 above, wires of natural fibers and plastics can also be employed.
2 The filter can also be reinforced in other places than at the
3 surfaces. It can, for example, be built on a foam material,
4 such as a plastic foam, which can support part of the entire fil-
5 ter.

6
7 The filters of the invention, especially in a non-
8 hardened or crosslinked form, should not be subjected to tempera-
9 tures in excess of 100°C, as such heat sterilization tends to
10 destroy the gel structure. It is, therefore, necessary in
11 utilizing the filters for biological processes to prepare them
12 sterilely from the beginning. On the other hand, it has been
13 found possible to harden or crosslink the filter during the prep-
14 aration by carrying out the gel formation in the presence of
15 Factor FXIII and calcium ions. Where Factor FXIII is to be pres-
16 ent, it is preferably present in an amount of at least 5 units
17 per gram fibrinogen, preferably at least 50 units per gram.
18 Calcium is present in a concentration of at least 20 mM.

19
20 A still stronger filter is obtained by effecting
21 crosslinking with one of the above-mentioned crosslinking agents,
22 especially a dialdehyde and particularly one of the formula
23 OCH-R-CHO , wherein R is an alkylene group of 1 to 8 carbon at-
24 oms, such as glutardialdehyde. The filter obtained in this
25 way can be heat treated in an autoclave and consequently steril-
26 ized.

27
28 The clotting parameters are above all the enzyme
29 concentration, e.g. between 100 and 3000 NIH units/L for throm-
30

bin and for the fibrinogen concentration between 0.1 and 70 g/l, preferably between 1 and 10 g/l, increased concentration giving a tighter gel. A tighter gel has a smaller pore size. Increased ionic strength also provides a tighter gel as well as a higher pH. It is preferred to carry out the gel preparation using a gel mixture having a pH of between 5.5 and 11, preferably between 6 and 9, and an ionic strength between 0.05 and 0.5. Gels formed at calcium ion concentrations between 0 and 20 mM are tighter.

Pore size is also affected by the temperature at which the clotting (gelation) is effected. A lower temperature of gelation means an increased clotting time, which in turn means that the resultant gel has a larger pore size. As a result of its larger pore size, it provides a greater rate of flow.

The gel of the invention can be used other than as a filter. One can dispose catalytically active substances such as catalytically active enzymes or catalytically active metals within the pores and thus use the pores' structure as a catalyst. The filter, therefore, can act more or less as a catalyst support for the catalytically active agent disposed therein. When the catalytically active agent is disposed within the pores, the resultant structure can be employed as a size selective catalyst converting only those components whose size is such as to freely pass through the pores of the catalyst support. Those materials retained in the surface of the gel are not catalytically converted.

By such a filter, one can conveniently effect enzymatic conversions, especially when the enzyme is immobilized

1 within the filter covalently, ionically or otherwise. Since
2 the gel structure is formed by the use of an enzyme, the filter
3 of the invention's chemical components is compatible with the
4 enzyme being employed as an enzyme catalyst. Thus, one can
5 use the filter of the invention for any of the following enzyme
6 conversions when the same contains the appropriate enzyme to ef-
7 fect that enzymatic catalysis: for reactions involving various
8 oxido-reductases; transferases, hydrolases, lyases, isomerases
9 and ligasis (synthetases). Hydrolases which have capacity of
10 degrading the protein strands in the gels cannot be used.

11
12 The method by which the enzyme or other catalytic
13 component is disposed within the filter, i.e., within the pores
14 of the filter, depends upon the nature of the enzyme. Prefer-
15 ably it is disposed by the use of a known enzyme immobilizing
16 agent followed by washing of the filter to remove extraneous
17 materials.

18
19 One can also dispose reactive cellulose^{or} components
20 within the pores of the gels. Upon reaction, low molecular
21 weight components may be released and subsequently eluted from
22 the gels. An example of such a type of reaction is production
23 of interferon by leukocytes after their reaction with Sendai
24 virus. As shown in this invention, both of these components
25 can be disposed within the pores of the gels.
26
27
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BRIEF DESCRIPTION OF DRAWINGS

The invention is described more in detail with reference to the enclosed drawing, in which:

Fig. 1 a shows molding of a filter according to the invention;

Fig. 1 b shows the filter arranged for filtering;

Figs. 2 a and 2 b show graphs of the flow as a function of the coagulation time at different pH with thrombin and Batroxobin, respectively;

Fig. 3 shows the turbidity of the fibrinogen solution (fibrinogen) as a function of the time after addition of thrombin;

Figs. 4 a and 4 b show the flow as a function of the coagulation time at different ionic strength of thrombin and Batroxobin, respectively;

Figs. 5 a and 5 b are graphs showing the relationship between protein concentration in the gel forming system and flow-rate.

Figs. 6 a and 6 b show the temperature plotted against the coagulation time and the flow, respectively, as a function of the coagulation time at different temperatures;

1 Fig. 7 shows the turbidity of the effluent (turbidity
2 in the effluent) in % as a function of the pore diameter in μm ;

3
4
5 Figs. 8 a, 8 b and 8 c are graphs plotting activation
6 of fibrinogen and clotting time (Ct).

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1 In order to more fully illustrate the
2 invention and the manner of practicing the same, the following
3 examples are presented.

4
5 EXAMPLE 1

6 METHODS AND MATERIALS

7 Human fibrinogen , Fraction 1-4 (7) was obtained from IMCO,
8 Stockholm, Sweden. The preparation, either a freeze-dried powder
9 or a wet paste, was 97-100% clottable (as determined spectro-
10 photometrically). A solution being 0.3 M in NaCl and 2% in
11 protein was prepared. This solution (50ml) was dialyzed against
12 0.3 M NaCl at 4° for 3 hrs. with changes of outer fluid (5 litre)
13 every hour. This dialyzed solution was further diluted with
14 deareated Tris-imidazole buffer (8) of pH between 6.5 and 8.2 to
15 protein concentrations between 1.2 and 5.0 g/l. In the final
16 dilutions the concentration of each Tris and imidazole was 0.02
17 M. When necessary increase in ionic strength was achieved by
18 inclusion of sodium chloride in the buffer. In order to inhibit
19 any trace of plasmin which may be generated, Trasylol (Bayer AG,
20 Germany) was added to a concentration of 5 KIE/ml to all buffers
21 and dialysis fluids.

22 In the gelation experiments the following procedures was
23 employed: To 3.65 ml of fibrinogen solution in a plastic tube
24 was added 70 µl of 1 M CaCl₂ solution, immediately followed by
25 50 µl of thrombin or Batroxobin solutions of varying concen-
26 trations. This mixture is called Reaction Mixture. The tubes
27 are rapidly inverted twice and transferred to the gel cup or to
28 the spectrophotometer cell within 10 seconds after addition of
29 enzyme. The further handling is described under separate
30 paragraphs.

1 Thrombin. In most experiments a bovine preparation prepared as
2 previously described (9) was used. Specific activity: 100-200
3 NIH units per mg. Control experiments with highly purified
4 (specific activity: about 2000 NIH units per mg human thrombin
5 (10) was performed in some instances.

6 Batroxobin (from *Bothrops marajoensis*) was obtained from
7 Pentapharm AG, Basel, Switzerland. Specific activity: 505 BU
8 per mg.

9 Hirudin was also obtained from Pentapharm AG. Specific activity:
10 1000 ATU per mg.

11 Reagents. All reagents used were of analytical grade.

12 13 PREPARATION OF GEL COLUMN

14 A solution of thrombin is added to a solution of fibrinogen
15 in a tris-imidazole buffer containing calcium salts with a pH of
16 between 6.5 and 8.2 and an ionic strength between 0.1 and 0.3
17 so that the final concentration is between 0.05 and 2.5 NIH-
18 units per ml. In other tests Batroxobin is used to obtain gel
19 formation in a concentration between 0.27 and 3.6 BU per ml.
20 The concentration of "Tris" and imidazole salts is each 0.02 M
21 and the concentration of calcium salt is also 0.02 M. The var-
22 iation in ionic strength is obtained by addition of NaCl.

23
24 Gels are also prepared at calcium ion concentration between
25 0 and 20 mM. With reduced calcium ion concentration the opacity
26 of the gels is increased. When thrombin is used to achieve the
27 gel formation the clotting time (Ct), also in the absence of
28 calcium ions is directly proportional to the flow rate and thus
29 also to K_s . When "Batroxobin" is used for the gel formation, the
30

1 stability of the gels in the absence of calcium ions is unsatisfactory, which makes flow measurements more difficult.

2 After addition of an enzyme such as thrombin or Batroxobin,
3 the solution is rapidly mixed and then poured into a cup, e.g.,
4 such a one shown in Fig. 1a. It is made of acrylic plastic^{x)} and
5 has an inside diameter of about 14 mm and a height of about 27
6 mm. The plastic cup is shown in Fig. 1a and the lower part of
7 the cup is provided with a nylon filter having a mesh size of
8 80 x 80 μ m. This filter is fastened by a plastic guard
9 ring. A film layer, e.g., "Parafilm[®]", is preferably applied
10 at the lower portion so that liquid is prevented from leaking
11 out of the cup. Immediately after introducing the solution
12 into the cup, a silk net with the mesh size 150 x 180 μ m is
13 adapted at the upper end and is fastened with a guard ring. The
14 liquid in the gel cup can, e.g., be about 1 mm over the net
15 surface. The cup is left at room temperature for at least 2
16 hours for complete gel formation, preferably in a place free of
17 vibrations.

18 After this time, the film is removed at the lower portion
19 of the cup, ^{and} with its contents of gel is placed in the holder A
20 according to Fig. 1b. A holder B is applied over the upper end
21 of the cup 1. At the upper end of the holder B there is an
22 opening as well as at the lower end of the holder A. The
23 holder B is filled with liquid (buffer or water) and a rubber
24 cork provided with a tube, which is connected with a rubber hose
25 is inserted into the opening. The rubber hose is connected with
26 a container for permeation solution which is allowed to fill the
27 rubber hose without air bubbles. The container (not shown in
28 the drawing) is placed at such a height that a suitable flow is
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x) (other materials can also be used such as nylon and pol-

obtained through the gel. The hydrostatic pressure is varied at different tests between 4 and 40×10^3 dynes/cm². ($4 \text{ and } 40 \times 10^{-2} \text{ N/cm}^2$)

The fibrinogen used for the preparation of the gels contains trace amounts of factor XIII, which is a transamidase. In the presence of this enzyme and calcium ions, covalent intermolecular cross-linkages between chains in the molecule units of the fibrin gel are formed. This is especially the case when thrombin is present as thrombin activates factor XIII.

An electrophoretic analysis of reduced fibrin from various gels in the presence of sodium-dodecyl sulphate shows that a complete cross-linking of the α and γ -chains of the fibrin takes place in the presence of thrombin. A partial cross-linking takes place in the presence of Batroxobin. The covalent cross-linkings formed in the presence of factor XIII contributes to the stabilization of the gel structure.

The silk net applied to the top of the gel cup and which is in intimate contact with the gel matrix is of great importance for the mechanical stability of the gels. Without this net or some other means for preventing collapse of the gel, the gel compound is destroyed in the flow tests, the gel collapsing in the central portion and a conical inward bend arising.

The silk net can, of course, be replaced with other nets, e.g., of cotton, nylon, iron or copper, which also stabilize the gel structure at pressures up to 40×10^3 dynes/cm². ($4 \times 10^{-2} \text{ N/cm}^2$)

Turbidity measurements

In parallel to the flow studies, the turbidity profile of the system was determined under identical conditions. In these experiments the Reaction Mixture (see under Fibrinogen) was

1 poured into a cuvette (5ml) of a recording spectrophotometer
2 (Beckman Acta III) and the turbidity (optical density) recorded
3 at 450 nm. After a lag-phase there was a rapid increase in tur-
4 bidity (cf. Fig. 8) which was accompanied by gelation. A
5 tangent was drawn to the steepest part of the sigmoidal curve.
6 Its intersection with the time axis is defined as the gelation
7 or clotting time (Ct). (Ct is about the same as the time for
8 visually observed turbidity increase in the gel cup.) In addit-
9 ion to Ct also maximum turbidity (OD-max) and rate of turbidity
10 increase (Δ OD/min) was recorded. The time required for
11 gelation to reach completion was judged from the turbidity
12 curve. This time ranged from 1 hr. to 2 hrs. for the high and
13 the low enzyme concentrations, respectively.

14 Determination of fibrinopeptides and cross-linking

15 Reaction Mixtures (see under Fibrinogen) were prepared in
16 several identical tubes. One of them was used for turbidity
17 measurement as described above. The other tubes contained each
18 1 ml of Reaction Mixture. The reaction in the latter tubes was
19 quenched at different times by addition of hirudin (2 ATU/ml)
20 and an equal volume of 8 M urea. Thereafter the fibrin (ogen)
21 was precipitated by addition of an equal volume of chilled
22 ethanol. The mixtures were kept on ice-bath for 2 hrs. and
23 thereafter the precipitates were secured by centrifugation,
24 dissolved in urea and used for SDS-gel electrophoresis. The
25 supernatants were used for radioimmunoassay (RIA) of FPA, FPB and
26 B β 15-42 was assayed using the recently developed method of
27 Kudryk et al.
28
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Viscosity was determined with a viscometer type Ubbelohde, having a flow time for water of about 290 sec at 25°C. It was calibrated against a standard (CNI. Cannon Instrument Company, Pa. USA).

Density was determined with a 5 ml pycnometer.

Pore size. The equation for calculation of average pore size of membranes (18) and acrylamide polymer gels (4) was applied:

$$r = \sqrt{\frac{8Ks}{\epsilon}} \quad (2) \quad (3)$$

where r is the average pore radius (in cm), and ϵ is the fractional void volume of the gel, i.e., the fractional volume of liquid in the gel. ϵ is calculated on the basis of protein concentration assuming a partial specific volume for fibrinogen of 0.72 (19), ϵ is in this case the fractional void volume for gels in which no water is bound to the gel matrix. However, the degree of hydration of fibrinogen in solution has been reported as high as 6 g per g protein. (20). Assuming that this water is retained by the gel matrix we also calculated ϵ for such hydrated gels.

Diffusion coefficient. The apparent diffusion coefficient of water in the gel was calculated from Ks according to Ticknor (21) and White (4).

$$D = \frac{R.T.Ks}{\epsilon.V.\eta} \quad (3) \quad (5)$$

where D is the diffusion coefficient (in $\text{cm}^2/\text{sec.}$). R is the gas constant (in ergs/mole-degree), T is the absolute temperature (in °K) and V is the molar volume of the permeant (in cm^3/mole).

1 Ionic strengths were calculated on basis of the molarity of the
2 electrolytes. Activity coefficients and degree of calcium
3 binding to protein were not taken into account.

4
5 Least square analysis was used for calculation of correlation
6 coefficients, slopes and intercepts. All lines shown in figures
7 were drawn accordingly.

8 RESULTS

9 Preparation and stability of gels

10 The flow studies were performed on gels which had been
11 formed at ambient temperature. The average temperature was
12 $24 \pm 2^\circ$. However, in each series of experiments the variation in
13 temperature never exceeded 2° . Preliminary experiments suggested
14 that this variation in temperature has a negligible effect on the
15 Ct of the system. In the permeation experiments, when not other-
16 wise stated, the flow-rates were corrected to 25° .

17 The silk net at the upper end of the gels stabilizes the
18 gel structures. Without support of the silk net, the gels will
19 yield to flow at the pressure applied (about 7×10^3 dynes/cm²), \leftarrow
20 The yielding is only noted at the center of the gel, since the
21 gel matrix adheres^{e)} firmly to the walls of the plastic cup.

22 The nets in the column do not significantly reduce the flow-
23 rate of liquid in columns without gels. We, therefore, assume
24 that also when the nets are in contact with gels they do not
25 restrict the area available for flow.

26 Before a flow experiment was started, the extent of
27 incorporation of fibrinogen into the gel matrix was determined.
28 This was done by determining the protein content in the void
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X 1 volume of the column (about 4 ml). The amount of protein, as
2 measured spectrophotometrically using the extinction coefficient
3 of fibrinogen (22), ranged between 1 and 3% of the total protein
4 used for gelation. When deemed necessary the non-clottable
5 portion was taken into account in calculations of the fibrin
6 content of gels.

7 The effect of changing permeant on the flow-rate of gels
8 was studied in some experiments. A representative series of
9 experiments is shown in Table I. The gel was first percolated
10 with buffer of ionic strength 0.21 (experiment I). On changing
11 the permeant to water (experiment II) an increase in flow-rate
12 occurred, which is larger than expected on the basis of the
13 viscosity change of the permeant. On return to the original
14 permeant (experiment III) the flow-rate decreased, but not
15 completely to the original value (experiment I). When buffer of
16 ionic strength 0.36 was percolated through the gel (experiment
17 IV) a small decrease occurred which was almost as expected on the
18 basis of the difference in viscosity between the two buffers.
19 When the permeant was again changed to water (experiment V) the
20 flow-rate increases to almost the same value as after the first
21 change to water (experiment II). These results suggest that the
22 final gel structure is not influenced by moderate changes in
23 permeant composition, but changes may occur on drastic changes
24 in ionic environment and these are not completely reversible.
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TABLE I 26

Flow Properties of Fibrin Gels with Different Permeants.

Gel formation: Tris-imidazole buffer pH 7.4, ionic strength 0.21, thrombin 0.8 NIH-units/ml, temperature 21°C and fibrinogen concentration 2 mg/ml.

Permeation; H_2O at 22°C - 23.5°C.

Experiment	Permeant	Flow, ml/hr	%
I	Tris-imidazole pH 7.4, $\sqrt{2}$ 0.21	3.177	100
II	H ₂ O	3.708	117
III	Tris-imidazole pH 7.4, $\sqrt{2}$ 0.21	3.385	106
IV	Tris-imidazole pH 7.4 $\sqrt{2}$ 0.36	3.271	103
V	H ₂ O	3.649	115

Flow pattern through fibrin gels

Viscous flow. In order to test if the flow obeyed Poiseuille's law, the flow-rate at different pressures ($4.5 - 5.6 \times 10^3$ dyne/cm²) \leftarrow for gels formed at pH 7.4, ionic strength 0.21 was determined, at three different thrombin concentrations (0.1-0.8 NIH units/ml). The Ks-range for these gels was 10^{-8} to 10^{-10} .

Permeation was in one experiment with the same buffer as above and in the other cases with water. In all cases the drop-rate decreased linearly with decreasing pressure. As shown in Table II for one of the gels, the flow-rate per unit pressure was almost independent of total pressure.

In another series of experiments the flow-rates were determined with permeants of different viscosities. The gels used

$$\left((4.5 - 5.6) \times 10^{-2} \text{ N/cm}^2 \right)$$

1 in these experiments were formed at pH 7.4, ionic strength 0.21,
2 at four fibrinogen concentrations. Thrombin as well as
3 Batroxobin were used as inducers of gel formation. Permeation
4 was performed at five different temperatures between 4.5°C and
5 40°C. In all cases there was a linear relationship between the
6 inverse viscosity of the permeant and the flow-rate. These
7 experiments suggest that the flow through the gels is viscous.
8 In addition Reynold's number was calculated and found to be
9 within the laminar region for all gels.

10 Diffusive flow. It was pointed out by Ticknor, J. Phys. Chem 62,
11 1483-5 (1958) that the equation for viscous flow is identical
12 in form to equations for diffusive flow, when the relationship
13 between diffusion coefficient (D) and viscosity according to Johnson and
14 Babb, Chem. Revs. 56, 387-453 (1956) is taken into consideration.
15 The relation between K_s and D is given in Equation 2⁵. In flow
16 experiments using water as permeant we calculated the apparent
17 diffusion coefficient for water at 22°C- 23°C. Even for the
18 tightest gels ($K_s > 10^{-10}$), the calculated D-values were 6-orders
19 of magnitude larger than the reported self-diffusion coefficient
20 of water at 25°C ($2.8 \times 10^{-5} \text{ cm}^2/\text{sec.}$). This supports the above
21 conclusion that the flow through the fibrin gels is predominately
22 viscous.
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TABLE II

Relationship Between Pressure and Flow-Rate.

Gelformation: pH 7.4; ionic strength 21, thrombin 0.1 NIH unit/ml temperature 23.5°C and fibrinogen concentration 2 mg/ml.

Permeation: H₂O, temperature 23.5°. Ks = 9×10^{-9}

Pressure, dyne/cm ² <->	%	Flow ml/hr	Flow per dyne per cm ² <-> ml/hr x 10 ³	%
5531	100	11.280	2.0394	100
5319	96.2	10.817	2.0337	99.7
5127	92.7	10.418	2.0320	99.6
4874	88.1	9.859	2.0228	99.2
4576	82.1	9.148	1.9991	98.0

Gel Permeability and clotting time (Ct)

There is a correlation between clotting time (Ct) of fibrinogen and enzyme concentration. We explored the relationship between Ct and permeability of the final gels. Therefore, at the same time as gels were prepared for permeability studies, the Ct of the gel forming system was determined in parallel experiments by turbidity measurements (see Methods).

pH. At a constant fibrinogen concentration and ionic strength, the flow-rates for both thrombin and Batroxobin gels were directly related to the Ct of the gel forming system over a wide range of Ct (17 sec - 500 sec). This applied to three different pH's (6.5, 7.4 and 8.2) as exemplified in Fig. 2. At all pH's there was a difference in slope between curves for thrombin as compared to those for Batroxobin.

- 28 -

$$< (1 \text{ dyne/cm}^2 = 1.0 \times 10^{-5} \text{ N/cm}^2) >$$

At each pH, the correlation coefficients (r) for six different Ct versus flow-rate curves (4 experimental points in each) were calculated. The mean r -values and their standard deviations (SD) were as follows: at pH 6.5, 0.9709 ± 0.0184 ; at pH 7.4, 0.9721 ± 0.0394 ; at pH 8.2, 0.9599 ± 0.0434 . There was no significant difference in r -values for thrombin and Batroxobin curves.

Ionic strength. In another series of experiments the ionic strength of the gel forming system was, at constant protein concentration, varied between 0.21 and 0.31. At all pH's (6.5, 7.4, 8.2) an increase in ionic strength from 0.2 to 0.3 resulted in a decrease in flow-rate by roughly one order of magnitude. This applied to both thrombin and Batroxobin gels.

Ct were prolonged with increasing ionic strength at all enzyme concentrations and pH's. At each ionic strength, however, there was for both thrombin and Batroxobin gels a linear relationship between Ct and flow-rate. The results at pH 7.4 is shown in Fig. 4. At all ionic strengths a difference in slope between curves for thrombin as compared to those for Batroxobin was noted.

At two ionic strengths, regardless of pH, r -values for six different Ct versus flow-rate curves (4 experimental points in each) were calculated. Mean r -values and SD were as follows: at ionic strength 0.21, 0.9851 ± 0.0208 and at ionic strength 0.26, 0.9511 ± 0.0470 . There was no significant difference in r -values for thrombin and Batroxobin curves.

Gel permeability and fibrinogen concentration

In a series of experiments we showed that the relationship between Ct and flow-rate applied to a wide range of protein concentrations in the gel forming system. These experiments were only performed at pH 7.4 and ionic strength 0.21. When Ct at a given protein concentration were plotted against flow-rates a linear relationship, similar to that shown in Fig. 3 (pH 7.4), was demonstrated at all fibrinogen concentrations (1.5 - 5.0 g/l). The plots for both thrombin and Batroxobin converged towards an intercept near the origin with decreasing clotting times. Like in the experiments shown in Fig. 2, the slopes for Batroxobin curves were steeper than those for thrombin at all protein concentrations. The r-values for 8 different Ct versus flow-rate curves (8 points in each) were calculated. Mean r-values and SD were as follows: for thrombin, 0.9800 ± 0.0157 and for Batroxobin, 0.9830 ± 0.0187 .

Table III shows Ct at different protein and enzyme concentrations in one series of experiments. In case of Batroxobin, increasing protein concentrations did not markedly influence Ct. However, in the case of thrombin there is a small prolongation of Ct with increasing fibrinogen concentrations.

The relationship between protein concentration in the gel forming system and flow-rate was next studied. Fig. 5 shows the result of one series of experiments. It is evident that there exists, at different enzyme concentrations, a linear relationship between flow-rate and inverse protein concentration. The curves ~~for~~^{of} thrombin and Batroxobin gels converge to a more or less common intercept near the origin with increasing protein con-

centration. The r-values for 15 different 1/C versus flow-rate curves (4-8 experimental points in each) were calculated. Mean r-values and SD_(standard deviation) were as follows: for thrombin, 0.9738 ± 0.0308 and for Batroxobin, 0.9711 ± 0.0356 .

It is apparent from Fig. 2 how the flow rate $\frac{Q}{t}$, at a constant hydrostatic pressure, is directly proportional to the coagulation time (Ct) of the thrombin-fibrinogen mixture at different pH. The coagulation time of the system is determined spectrofotometrically in a separate test under otherwise identical conditions. The optical density OD at 450 nm is determined. At gel formation the turbidity of the solution increases rapidly as shown in Fig. 3. The tangent of the steepest portion of the curve intersects the time axis at a distance designated as coagulation time Ct. As there is a direct relation between Ct and flow^w rate $\frac{Q}{t}$, Ks is also directly correlated with Ct according to equation 1.

It is apparent from Fig. 4 that the flow rate of gels formed at different ionic strength is always directly correlated to the Ct of the enzyme-fibrinogen solution used in the gel preparation. In addition the great influence on the flow rate at a change of the ionic strength is pointed out.

As is apparent from Fig. 5, the flow rate $\frac{Q}{t}$ is inversely proportional to the fibrin concentration (fibrinogen concentration) in the gel. Thus, according to equation 1, Ks will also be inversely proportional to the fibrinogen concentration.

The flow is dependent on the temperature, as according to equation 1, the flow is inversely proportional to the viscosity of the permeation solution. The temperature in gel formation is

1 also of importance as a constant enzyme concentration, Ct is
2 reduced at a higher temperature. This is apparent from Fig 6a.
3 However, the flow rate in gels formed at different temperatures
4 is directly proportional at Ct at the relative temperature, as is
5 evident from Fig. 6b.

6 The columns prepared in the way schematically illustrated
7 in Fig. 1 are of small dimensions ($1.5 \text{ cm}^2 \times 2.6 \text{ cm}$). Similar
8 qualitative results are observed with gel columns of greater
9 dimensions ($5 \text{ cm}^2 \times 12 \text{ cm}$). When nothing else is indicated, the
10 smaller type of column is used in the tests.

Example 2Standardization of pore size with latex particles of a known size.

Spherical latex particles of diameters between 0.085 ± 0.0055 (SD) μm (SD = standard deviation) and 0.198 ± 0.0036 (SD) μm from Dow Chemicals, USA, were used in the tests. A number of gels formed at pH 7.4, and at two different ionic strengths, were used. In the tests, C_t varied from 23 to 314 seconds. The theoretical radius was calculated for each gel according to equation 3 assuming that a cylindrical vertical capillary system was present.

Fig. 7 shows two series of tests. In series I the ionic strength was 0.23 during the gel formation and in series II 0.21. The gel columns were equilibrated with water. After this, suspensions of particles were applied to the gels. In series I the particle size was $0.085 \mu\text{m}$ and in series II $0.198 \mu\text{m}$. The particles were slurried in water to a concentration of 0.1% (weight/volume). The turbidity (at 450nm) of the effluent was determined. It was then possible to establish by means of the turbidity values if the latex particles had passed the filter.

In Fig. 7 the turbidity has been expressed in % of maximum turbidity of the effluent. As is apparent from Fig. 7 the turbidity of the effluent increases above a certain theoretical pore size of the gel. At an additional increase in pore size more particles will pass through the gel (filter) and over a certain pore size a constant amount of particles permeate the gels. The difference in theoretical pore size between no and

1 complete permeation is a measure of the sum of pores and
2 particle variation. The pore size at 50% permeation is an ex-
3 pression of the average size of pores and particles. If the
4 total variation in pore size is within the range of the average
5 particle size ± 3 SD it can be assumed that the pore size in the
6 gel is uniform.

7 In Fig. 7 the variation in particle size (average size ± 3
8 SD) has been shown with a horizontal line 50% permeation. It is
9 apparent that the total variation can, to a large extent, be ex-
10 plained by the particle variation. It can be concluded from this
11 that the pores in the gels are rather uniform. It is also
12 apparent from Fig. 7 that the theoretical average pore size is
13 about of an order (one ten power) greater than the real effective
14 particle size. Thus, calculation of the pore size according to
15 equation 3 only gives relative values for the pore size.

EXAMPLE 3Passage of proteins and dextran through fibrin gels

Various protein solutions were (applied) to fibrin gels prepared in the way described in Example 1. The gel formation was carried out at room temperature (21° - 25°C). In most cases, the buffer used in gel formation had the same composition as the buffer used for permeation. The filtration tests took place at room temperature (22° - 25°C). When nothing else is indicated, the volume of the gels was $1.47 \text{ cm}^2 \times 2.48 \text{ cm} = 3.65 \text{ ml}$. The tests were carried out on different days and with different fibrinogen preparations. Thus, it is not possible to make a comparison as to the pore size between different tests. Table 1 shows the proteins tested with respect to filtering ability through fibrin gels of different porosities. It is apparent from the table, that proteins, including those having a very high molecular weight, are filtered even through gels having small pore sizes. A high molecular weight polysaccharide ("Blue Dextran") shows the same filtration properties as the proteins. The table shows that the yield of proteins in the eluate is high, from which it appears that at least at room temperature the interaction between gel matrix and proteins is small. This also applied to such proteins as fibrinogen, fibronectin and the factor VIII complex.

TABLE I

Filtration of proteins and particles through fibrin gels

Test	Diameter or mol. weight	Permeation Buffer, ml	Yield, %	Pore diam. a) μm	Ct s	Protein g/l	Gel formation $\frac{r}{2}$	pH	Enzyme
Human serum	-	TI buffert + Ca^{2+}	98.2	2,12-4,86 (0,125-0,286)	16-230	3,42	0,21	7,40	T
Human plasma	-	TI buffert - Ca^{2+}	101.1	0,288	260	4,56	0,26	7,40	T
Fibrino- gen (4g/l)	340000	TI buffert - Ca^{2+}	93,8	4,34 (0,255)	124	2,157	0,21	7,40	T
Fibrino- gen (4g/l)	340000	TI buffert + Ca^{2+}	97.8	2,33 (0,137)	66	2,157	0,21	7,40	B
Fibro- nektin (2,3g/l)	440000	TI buffert - Ca^{2+}	109	2,30 (0,135)	430	2,274	0,21	7,40	T
Antihæ- mophilic factor (FVIII)b	2-6x 10 ⁶	TI buffert + Ca^{2+}	99.8	2,48 (0,146)		3,000	0,21	7,40	T
		1.0	63	1,08 (0,064)		5,000	0,26	7,40	
Ferri- tin (15g/l)	2x10 ⁶	TI buffert + Ca^{2+}	103.8	0,276 (0,016)	440	4,56	0,26	7,40	T

a) The theoretical diameter was calculated according to equation 3. The effective diameter through calibration with latex particles.

The effective pore diameter is given within brackets. (Based on a ratio $\frac{\text{theoretical}}{\text{effective}}$ of about 17)

b) The volumes of the gel column; 4,9 cm x 11 cm = 53.9 ml.

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TABLE 1 (cont.)

Test	Diameter or mol. weight	Permeation Buffer	Sample ml	Yield %	Pore diam. μ m	Gel formation Gt s	$\frac{P}{2}$	pH	Enzym
Human erythrocytes (11g/l)	3×10^6	TI buffer $\times Ca^{2+}$	0.2	97.7	0.276 (0.016)	440	0.26	7.40	T
Human red blood corpuscles 5×10^6 /ul	7 μ m	Physiolo- gical common salt solution $-Ca^{2+}$	0.1	0	3.60 (0.212)	255	0.21	7.40	T
Human Platelets (4×10^5 /ul plasma)	2~4 μ m	TI buffer $-Ca^{2+}$, +10m M EDTA	0.3-5	0	4.86 (0.286)	228	0.21	7.40	T
Rat liver mitochondria	0.5 μ m	TI buffer $-Ca^{2+}$ +0.25M sy- kros, +10m M EDTA	0.3	0	4.40 (0.259)	524	0.21	7.40	T
E. Coli	0.8x1.2 μ	TI-buffer $-Ca^{2+}$	45	0	1.78 (0.105)	24	0.21	7.40	T
Sundai-vi- rus (640) hemaggluti- nation units /ml	0.15 μ m	TI buffer $-Ca^{2+}$, + 1% BSA	I 0.2 II 0.2 III 0.2	0 50.3 95.2	0.284 (0.017) 2.36 (0.139) 4.46 (0.262)	33 19 137	0.233 0.21 0.21	7.40 7.40 7.40	T T T
Sundavirus filtered through harden- ed and autoclaved thin layer fibrin gel (see Example 6 and Table 2-III) in the filtrate - on the filter	0.15 μ m	TI buffer $+Ca^{2+}$	5	-	0.268 (0.016)	60	0.26	7.40	T

2
3 Filtration of suspensions of red blood corpuscles through
4 fibrin gels

5
6 Fibrin gels were prepared in the way described in Example I
7 and the conditions of gel formation is shown in Example 3. A
8 small amount (0.2 ml) of human blood was applied to a gel column.
9 Continued filtration was carried out at room temperature (22°-
10 25°C) under the conditions shown in Example 3. The blood
11 corpuscles did not pass through the fibrin gel. This was ex-
12 pected as the diameter of the red blood corpuscles (7-8 μ m)
13 is much larger than the effective pore diameter of the fibrin
14 gel.

1 EXAMPLE 5a

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3 Filtration of plasma rich in platelets through fibrin gels

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5 Plasma rich in platelets (PRP) was prepared from blood by cen-
6 trifugation for 4 minutes at 120g, the blood being drawn in
7 citrate solution to prevent coagulation. It was cetrifugated at
8 2000 g for 5 minutes to remove the remaining red blood corpuscles
9 and EDTA at a concentration of 10 mM was added to the PRP.
10 0.5 ml of the PRP was applied to a fibrin gel column prepared in
11 the way described in Example I. The conditions of gel formation
12 is shown in Example 3 and filtration was continued under the
13 conditions shown in Example 3. To prevent aggregation of the
14 platelets and their adhesion to the gel matrix, EDTA (10 mM) was
15 added not only to PRP but also to the solution which was filtered.
16 No platelets could be demonstrated in the eluate from the fibrin
17 gel column. This was expected as the diameter of the platelet
18 lies between 2 and 4 μ m, which is considerably more than the
19 effective pore size of the gel.
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1 EXAMPLE 5b

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2
3 Separation of mitochondria from fragments of liver cell by
4 filtration through fibrin gels
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6 Liver cells of a rat were homogenized in a homogenizator
7 according to Potter-Elvehjem. Separation of cell fragments was
8 achieved by differential centrifugation in known manner. The
9 mitochondria were slurried in a buffer solution containing Na-
10 EDTA (10^{-4} M) and succrose (0.25M). 0.3 ml of the resulting
11 suspension was applied to a fibrin gel column prepared in the way
12 described in Example 1. The conditions of gel formation is shown
13 in Table I and filtration was continued under the conditions
14 indicated in Table 1. No mitochondria could be demonstrated in
15 the eluate, which was as expected, since their diameter is about
16 $0.5 \mu\text{m}$, thus considerably bigger than the effective pore size
17 of the gel.
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2
3 Separation of Sendai-virus by filtration through fibrin gels4
5 Sendai virus is a virus specific to mice which is used for pre-
6 paration of interferon in human lymphocyte cultures. A partially
7 purified virus preparation (640 hemagglutination units/ml) was
8 used in the tests.9 0.2 ml of the virus suspension was applied to each of three
10 fibrin gel columns prepared in the way described in Example 1.
11 The conditions of the gel formation appear from Table 1 and
12 filtration was continued under the conditions shown in Table 1.
13 No hemagglutination activity could be demonstrated in the eluate
14 from column I; 50% of hemagglutination activity were demonstrated
15 in the eluate from column II and 95% of the hemagglutination
16 activity of the virus particles was demonstrated in the eluate
17 from column III (see Table 1).18
19 After filtration the silk nets at the upper part of the three
20 columns were washed with a buffer solution (containing 1 % of
21 bovine serum albumin, BSA) and the hemagglutination activity of
22 the washings was analyzed. In the washing liquid from columns I
23 100% of the hemagglutination activity was found; in the washing
24 liquid from column II 25% of the activity was found and in the
25 washing liquid from column III no activity was found.26 The particle diameter of Sendai virus is stated to be about
27 0.15 μ m. The tests show that when the effective pore radius is
28 more than 0.15 μ m the virus particles pass through the gel. When
29 the effective pore radius of the gel is less than 0.15 μ m a re-
30 tention of the particles will, on the other hand, occur.

EXAMPLE 7

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Separation of Eschericia Coli (E. coli) by filtration through
fibrin gel.

E. coli is an elongated intestinal bacterium of the approximate dimensions $0.8 \times 1-2 \mu\text{m}$. A suspension of E. coli in tris-imidazole-buffer, free of calcium and with pH 7.4 and ionic strength 0.21, was prepared (see Example 1). The suspension contained between 10^7 and 10^8 bacteria/ml. 45 ml of the suspension were supplied to a fibrin gel column of the dimensions $5 \text{ cm}^2 \times 11 \text{ cm}$ prepared in the way described in Example 1. The conditions of the gel formation and the filtration are shown in Table 1. The flow rate was 31 ml/h. No bacteria passed through the gel, determined by turbidity measurements of the eluate from the column. The flow rate at constant pressure was less at the end of the test than at its beginning. Assuming an unchanged K_s , the reduction of surface corresponding to the reduction in flow can be calculated according to equation 1. According to this calculation the surface had been reduced to 58%. Thus, one might expect that the bacteria were enriched on the upper gel surface. By washing the silk net attached to the upper part of the gel with buffer solution 99% of the bacteria applied to the gel were found in the washing liquid.

The test shows that E. coli cannot pass through gels having a pore diameter which is considerably less than the smallest diameter of the bacteria.

EXAMPLE 8

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Preparation of gels with reinforcement of porous plastic

In the foregoing examples nets of silk, plastic or metal adapted to the upper and lower portions of the gel have served as stabilizing structure of the fibrin gels. A corresponding stability can also be obtained in such a way that the fibrin gel is cast into a porous plastic, e.g. polyurethane, polyester or some similar porous plastic material, preferably one which is wettable by water.

In this example a foam plastic of polyurethane ("Regilen 40 AG") of a pore size 0.4 mm has been used. The gels were cast in a special apparatus. This consisted of a cylindrical plastic chamber in which the porous plastic had been introduced; the plastic was accommodated in a ring of acrylic plastic (height 2 cm and diameter 9 cm). The apparatus (chamber) had an opening at the upper and lower end, respectively. One opening was connected to a vacuum pump and the other opening was kept closed. The chamber was evacuated by means of the vacuum pump. After this, the valve connecting the chamber with the vacuum pump was shut off. A fibrinogen-thrombin solution was subsequently allowed to fill the chamber rapidly through the valve in the opposite opening. The valve was thereafter closed and the chamber was left for 2 hours, so that the fibrinogen solution in the porous plastic material should be completely converted to a fibrin gel. The clotting parameters of the thrombin-fibrinogen mixture was shown in Table 2. For comparison, a gel was also prepared in the way described in Example 1. In Table 2 the Ks -value of this latter

1 gel is also shown. After complete gel formation the chamber was
2 opened and the plastic cake with fibrin gel(including its plastic
3 frame) was taken out. It was transferred to a special filter
4 chamber. The framed ring, in which the plastic material and the
5 gel were accomodated, fitted tightly to the edges of the filter
6 chamber through two O-rings. The upper lid of the chamber was
7 provided with an inlet for the liquid to be filterd and a vent-
8 ilating valve to let our the air above the gel surface. In the
9 lower portion of the chamber there was an outlet for collecting
10 the filtered liquid. A buffer solution with the composition
11 shown in Table 2, was filtered through the gel cake. The Ks
12 value was calculated according to equation 1 (Table 2). As is
13 apparent from the table the Ks-value of the gel, cast in plastic,
14 is of the same order as the gel prepared according to Example 1.
15 The partial specific volume of the plastic material in the gel
16 cake is 0.03 which means that the plastic matrix reduces the
17 surface available for flow only to a small extent.

3 Preparation of gels in a cellulose matrix

4
5 Cellulose materials can also be used as reinforcing agent
6 (supporting substance). In this example, a porous cellulose
7 compound ("Wehex cloth") is used as reinforcing agent of the
8 fibrin gel. It had a thickness of 0.2 - 0.3 cm. Circular pieces
9 of a radius of about 3 cm were wetted with a thrombin-fibrinogen
10 solution. The cellulose pieces then swelled to about double
11 thickness. The partial specific volume of the swollen cellulose
12 compound was 0.04. Immediately after swelling which lasted for
13 about 2 - 4 seconds the pieces were placed on the filter disc of
14 a Büchner funnel. Measures were taken so that the pieces fitted
15 tightly to the edges of the funnel. The openings of the funnel
16 were covered with "Parafilm" and the funnel was left at room
17 temperature for 2 hours in order to obtain a complete fibrin
18 formation in the pores of the cellulose. Buffer solutions, the
19 composition of which is shown in Table 1, were filtered through
20 the gels. The Ks-value of the gels which are cast in cellulose
21 is of the same order of magnitude as control gels prepared without
22 reinforcing substance.
23
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EXAMPLE 10Preparation of fibrin gels in thin layers for filtration

In this example it is shown that fibrin gels in thin layers with reinforcement only on the lower surface can be used for filtration. About 10 ml of fibrinogen solution in tris-imidazole buffer with pH 7.4 were mixed with a thrombin solution. The mixture was thereafter poured into a Petri cup the bottom of which was covered by a damp silk cloth. The cup was covered with a lid and was left for 2 hours for a complete gel formation. The thickness of the gel layer was 2 mm. The clotting parameters of the gel is shown in Table 2. The filter was thereafter attached to a "Millipore" filter support provided with a funnel. The funnel was filled with buffer solution and the flow rate was determined. As is apparent from Table 2, the Ks-value is of the same order or magnitude for a corresponding fibrin gel prepared according to Example 1. However, the filter showed in course of time gradually diminishing Ks-values, which presumably is due to compression of the gel matrix during the flow.

EXAMPLE 11

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Stabilization of gels by treatment with dialdehyde

In this example it is shown that gels prepared according to Examples 1, 8 and 10 can be stabilized by treatment with dialdehyde.

A. A gel prepared according to Example 1 was first equilibrated with water and then brought into equilibrium with 0.014 M phosphate buffer solution with pH 7.2 in 0.15 M NaCl (phosphate buffered saline solution PBA). 2 - 4 column volumes of a 1% glutaraldehyde solution were then allowed to filter through the gel in the course of 10 minutes - 2 hours. After this the gel was washed with several column volumes of PBS and then with water. The column was finally equilibrated with tris-imidazole buffer and flow measurements were carried out. The Ks-value is almost unchanged after treatment with glutar dialdehyde. After the flow measurements, the gel was taken out and treated for 72 hours with 8 M urea containing 1% of sodium dodecyl sulphate (SDS). The gel was then reduced with 1% dithiotreitol in a way known per se. Polyacrylamide gel electrophoresis in the presence of SDS showed in comparison with non-stabilized gels the absence of free fibrin chains (fibrinogen chains), which can be interpreted as a proof that glutar dialdehyde had cross-linked the chain units of the fibrin structure.

B. A gel prepared in porous plastic according to Example 1* was first washed with a tris-imidazole buffer solution free of calcium and was then brought into equilibrium with a 0.014 M

phosphate buffer solution with pH 7.2 in 0.15 M NaCl (PBS).

Two column volumes of a 1% glutar dialdehyde solution were then passed through the gel cake (column) in the course of 10 minutes.

The gel cake was then washed with several column volumes of PBS and then with water. Finally the column was brought into equilibrium with tris-imidazole buffer and flow measurements were

carried out. These are shown in Table 2. As is apparent from the Table the K_s -value is only slightly changed after the treatment with glutar dialdehyde and is of the same order of magni-

tude as a gel prepared according to Example 1. The gel stabilized with glutar dialdehyde was then autoclaved at 120°C for 20

minutes at a pressure of 1.4 atm[←]. After autoclaving the flow of buffer solution was again tested through the gel cake. As is apparent from Table 2, autoclaving has influenced the flow properties of the gel only to a small extent. Cracks in the gel would have caused drastic increase of the flow through the gel.

C. A fibrin gel prepared according to Example 10 was transferred to a cup with 500 ml water to remove buffer salts by diffusion. After 2 hours the gel was transferred to a cup with a new portion of water. After 2 hours the gel was transferred to a cup with 500 ml phosphate buffer solution with pH 7.2 in 0.15 M NaCl (PBS) and was left over night. The gel was then transferred to a Petri cup containing 50 ml of 1% glutar dialdehyde. After 2 hours the glutardialdehyde solution was exchanged for a new portion of the same liquid. After additional 2 hours the gel was transferred to a cup with water and washed in the way described above. After washing with water the gel was transferred to a cup with tris-imidazole buffer solution. After 2 hours the washing liquid was exchanged for a new portion and after addit-

1 ional 12 hours the gel was transferred to a "Millipore"-filter
2 carrier with a funnel. As a comparison, measurements were carried
3 out with a gel prepared in the same way except the treatment with
4 glutar/dialdehyde. Directly after casting, this gel was trans-
5 ferred to a "Millipore" filter container for flow measurements.
6 As is apparent from Table 2 the flow through the vulcanized
7 filter was comparable with that through the non-vulcanized filter
8 at the start of the flow measurement. However, at the end of the
9 measuring period, the K_s -value of the nonstabilized filter had
10 been reduced to a large extent which was not the case with the
11 vulcanized filter. After the flow measurement the filters were
12 sterilized through autoclaving of the filter (and the filter
13 apparatus) at 120°C for 20 minutes at the pressure $1.4 \text{ atm.} \leftarrow$
14 Flow measurements were carried out after the heat treatment and
15 the K_s -values are shown in Table 2..

16 No flow could be demonstrated through the nonstabilized
17 filter. On the other hand the vulcanized filter showed K_s -values
18 of the same order before as well as after autoclaving.

19 5 ml of a suspension of Sendai-virus were supplied to the
20 vulcanized filter. Filtration was carried out by means of a
21 water suction. When the liquid had passed the filter, additional
22 5 ml of buffer solution were passed through the filter. This
23 was repeated twice. The filtrate was tested for hemagglutina-
24 tion activity. Inconsiderable hemagglutination activity could be
25 demonstrated. The upper surface of the filter was washed with
26 several portions of buffer solution. The washing liquid was
27 opalescent and its hemagglutination activity corresponded to a
28 yield of virus particles of almost 100%.

29 These examples show that the filters can be stabilized with
30 a dialdehyde such as glutar/dialdehyde.

Type of filter	Permeation		K _{S2} cm	Diameter µm	Ct, s	Gel formation		pH	temp, °C
	Buffer	Pressure ₂ (10 ⁻⁵ N/cm ²)				fbg. conc. g/l	$\frac{m}{2}$		
I a Fibrin gel in foam plastic	TI ₂ ⁺ +Ca ²⁺	-	5.82x10 ⁻⁹	4.38 (0.258)	171	2.478	0.21	7.4	23
b Vulcaniza- tion	"	-	5.20x10 ⁻⁹	4.14 (0.243)	"	"	"	"	"
c Vulcaniza- tion and steri- lization	"	-	1.39x10 ⁻⁹	2.14 (0.126)	"	"	"	"	"
d Control	"	-	3.15x10 ⁻⁹	3.17 (0.264)	"	"	"	"	"
II Fibrin gel in cellulose sponge Control	TI ₂ ⁺ +Ca ²⁺	3430	0.61, 0x10 ⁻¹¹	0.139-0.180 (0.008-0.011)	60	9.864	0.26	7.4	24
	"	29400	1.14x10 ⁻¹¹	0.192 (0.011)	"	"	"	"	"
III a Thin layer fibrin gel	TI ₂ ⁺ +Ca ²⁺	7350	1.0-2.5x10 ⁻¹¹	0.180-0.284 (0.011-0.017)	60	9.864	0.26	7.4	24
b Vulcaniza- tion	"	7350	3.6x10 ⁻¹¹	0.343 (0.020)	"	"	"	"	"
c Vulcaniza- tion and sterilization	"	7350	2.24x10 ⁻¹¹	0.269 (0.016)	"	"	"	"	"
d Vulcaniza- tion and sterilization	"	9.86x10 ⁵	3.52x10 ⁻¹²	0.107 (0.0063)	"	"	"	"	"
e Vulcanization and sterilization	"	7350	1.66x10 ⁻¹¹	0.232 (0.014)	"	"	"	"	"
f Control	"	29400	1.14x10 ⁻¹¹	0.192	60	9.864	0.26	7.40	24

T₂ = tris-imidazol buffer

See also explanation to Table I.

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1 1. A fibrin gel containing therein at least one catalytically active substance.

5 2. A fibrin gel according to claim 1 wherein said gel has substantially uniform pore sizes and contains means for retaining the shape of at least one surface of the gel against deformation when contacted by a flowing medium.

10

 3. A fibrin gel according to claim 2 wherein said means for retaining the shape of at least one surface of said gel is disposed on at least the upper surface of said gel.

15

 4. A fibrin gel according to claim 3 wherein said means for retaining the shape of at least the upper surface of said gel comprises a foraminous sheet member or a foam.

20

 5. A fibrin gel according to claim 1 wherein said fibrin gel is itself disposed in a porous-plastic material

25

 6. A fibrin gel according to claim 1 wherein said fibrin gel is disposed in a cellulose matrix.

30

 7. A fibrin gel according to claim 5 wherein said porous plastic material is a porous plastic that is wettable by water.

35

1 8. A fibrin gel according to claim 7 wherein said
porous plastic material is polyurethane.

5 9. A fibrin gel according to claim 7 wherein said
porous plastic material is polyester.

10 10. A fibrin gel according to claim 1 wherein said
fibrin gel has substantially uniform pores of a theoretical diam-
eter of 0.003 to 1 μ m.

15 11. A fibrin gel according to claim 10 wherein said ge.
has pores of a theoretical diameter of 0.009 to 0.3 μ m.

20 12. A fibrin gel according to claim 1 wherein said
catalyst is a catalytically active enzyme or a catalytically act-
ive metal.

25 13. A fibrin gel according to claim 12 wherein said
catalyst is a catalytically active metal.

30 14. A fibrin gel according ro claim 13 wherein said cat
alyst is a catalytically active enzyme.

1 15. A fibrin gel according to claim 14 wherein said
enzyme is an enzyme selected from the group consisting of an
oxido-reductase, a transferase, a hydrolase, a lyase, an isom-
5 erase, and a ligase except a hydrolase which has the capacity of
degrading a protein strand in a gel.

10 16. A fibrin gel having disposed therein a reactive
cellular component.

15 17. A fibrin gel according to claim 16 wherein said
fibrin gel contains leucocytes.

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FIG. 1a.

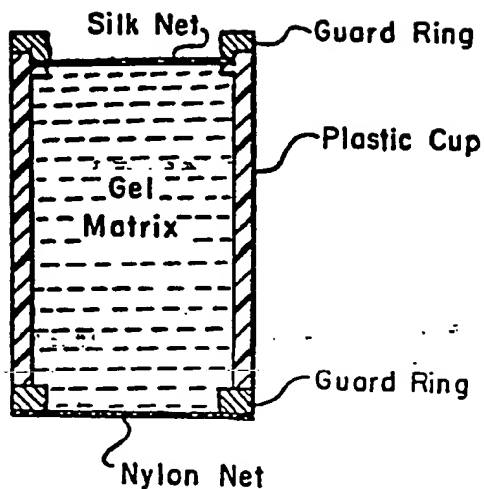


FIG. 1b.

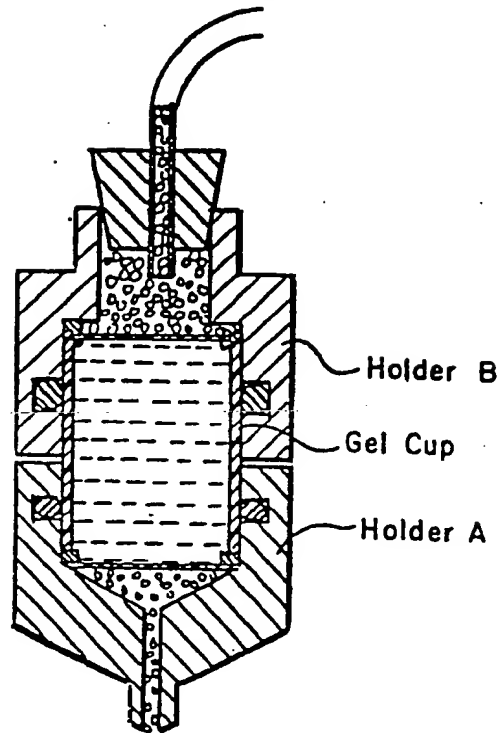


FIG. 8a.

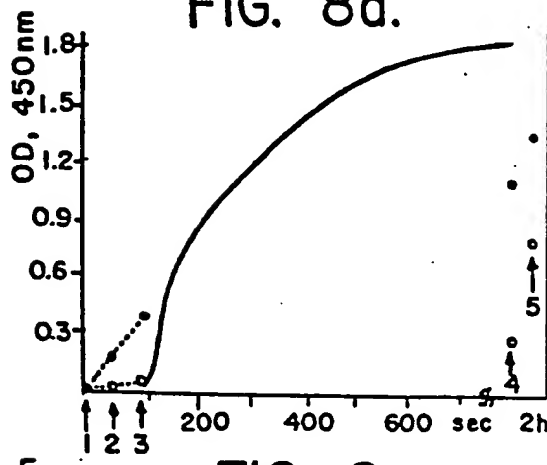


FIG. 8b.

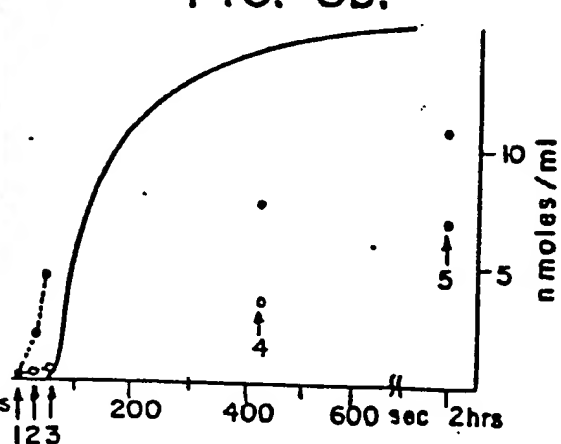
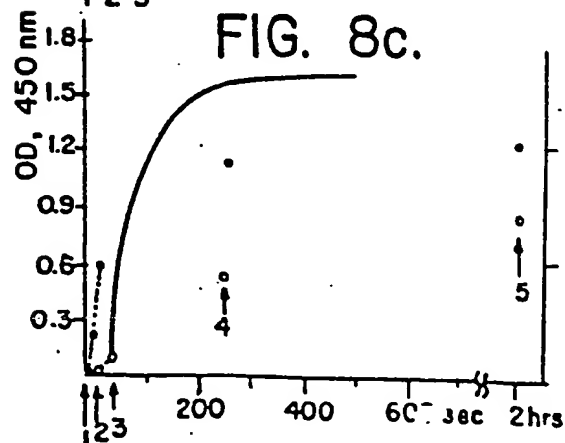


FIG. 8c.



Turbidity profile and release of
fibrinopeptides during gelation

- Optical density
- FPA
- FPB

FIG. 2b.

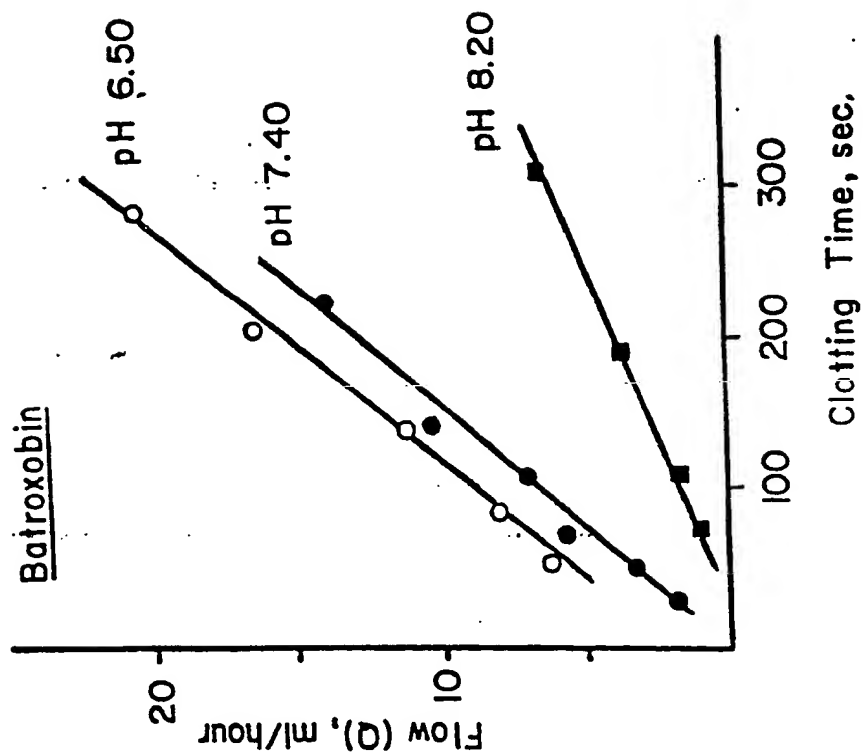
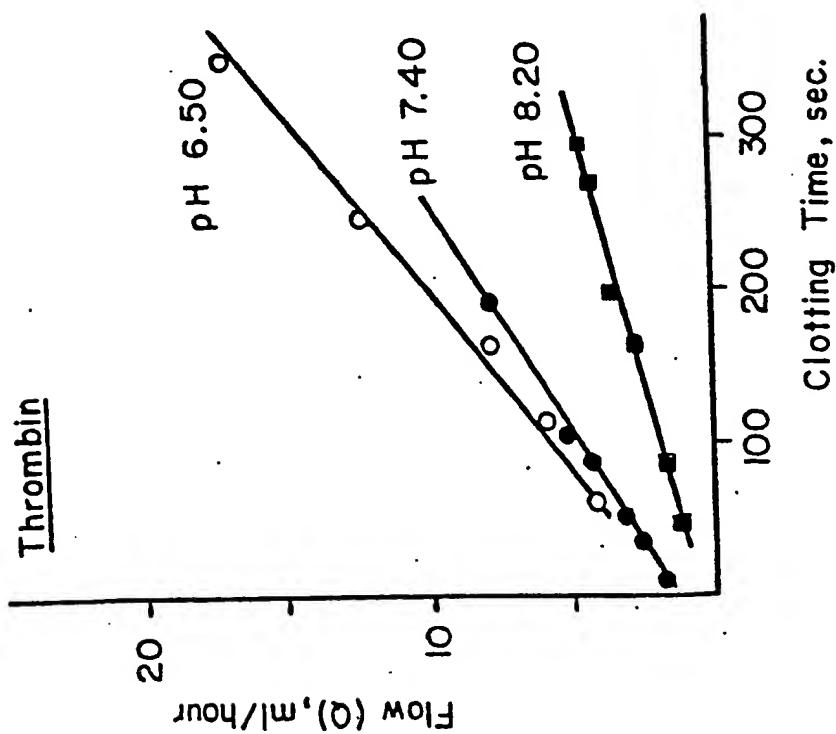
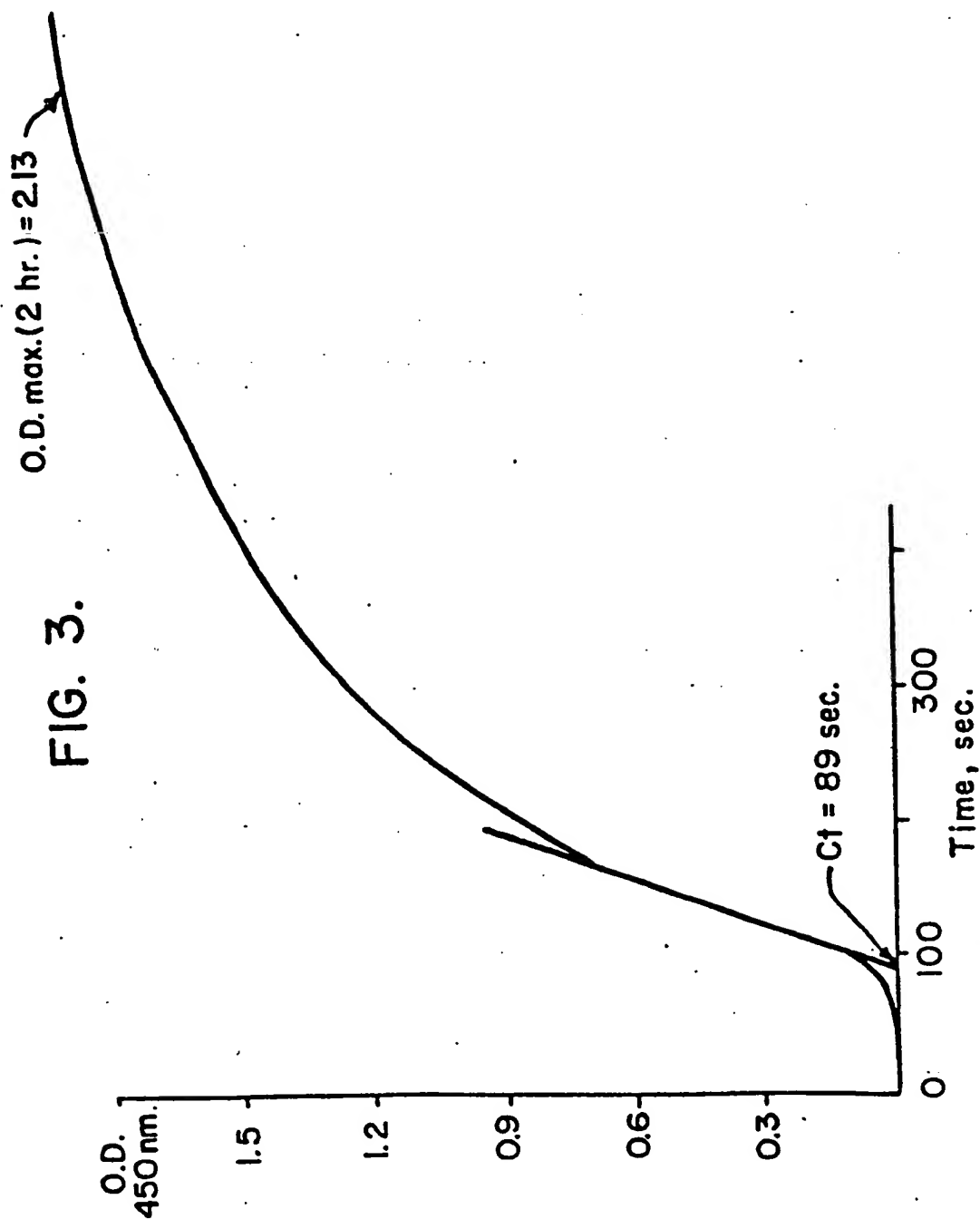


FIG. 2a.



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FIG. 4b.

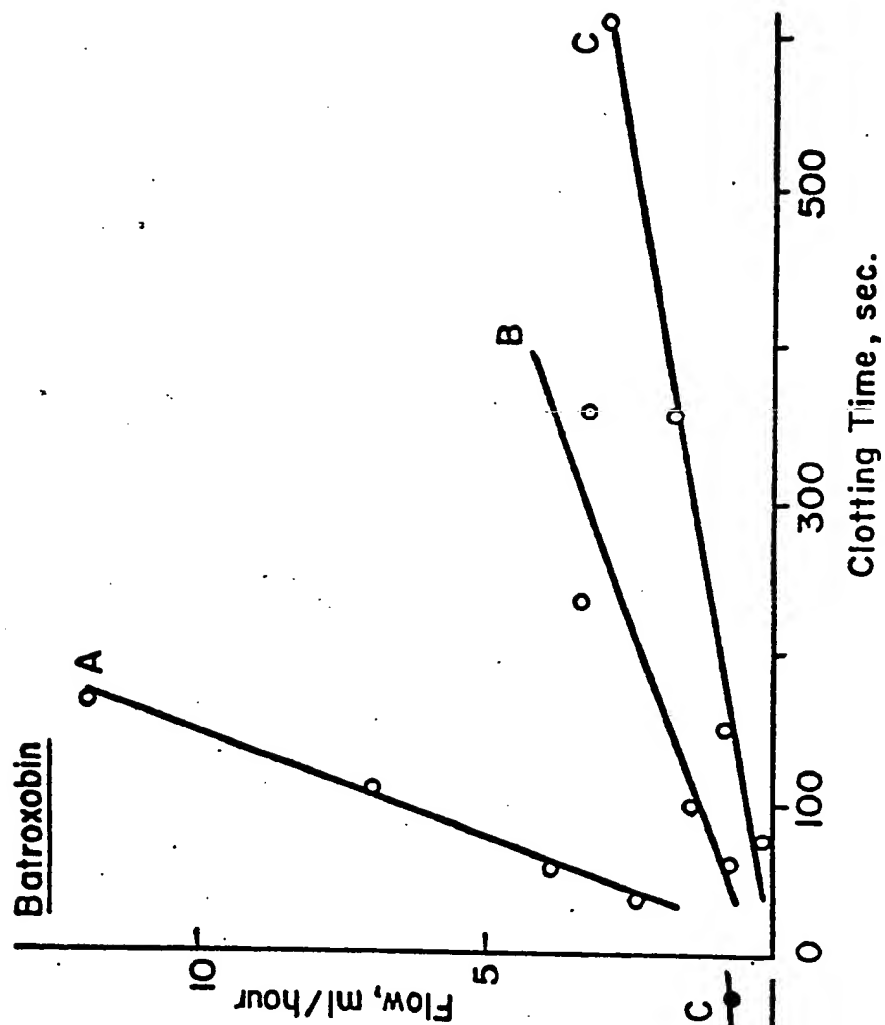


FIG. 4a.

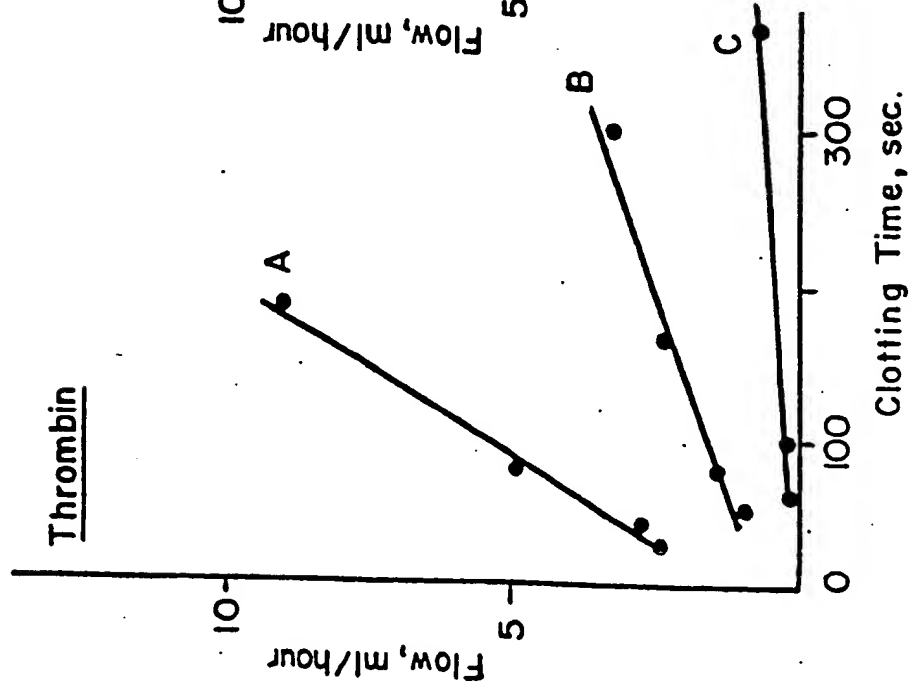


FIG. 5b.

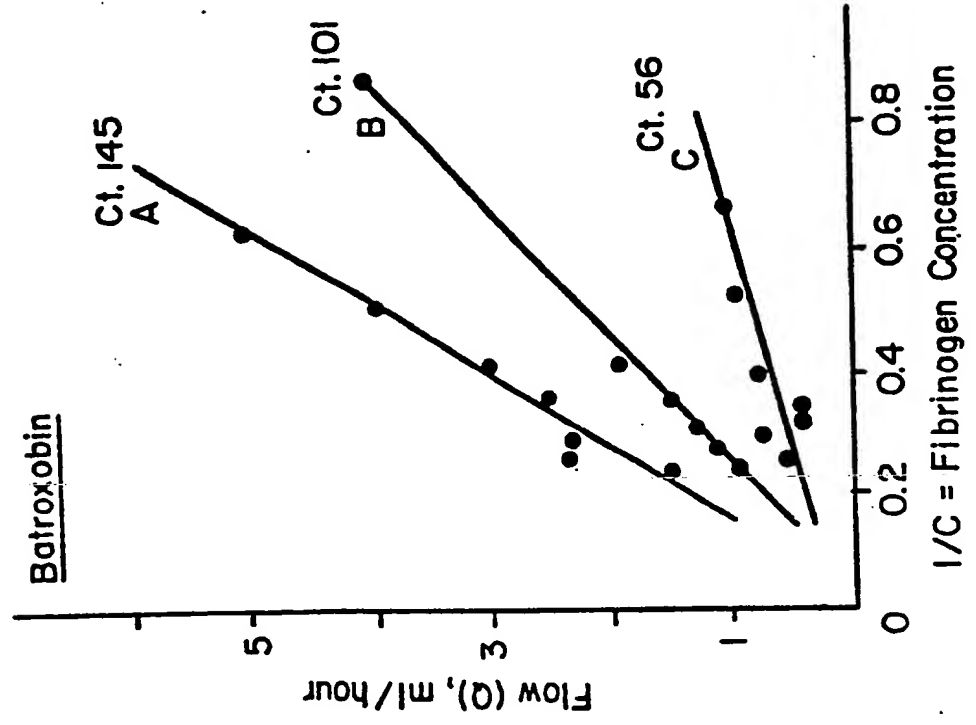
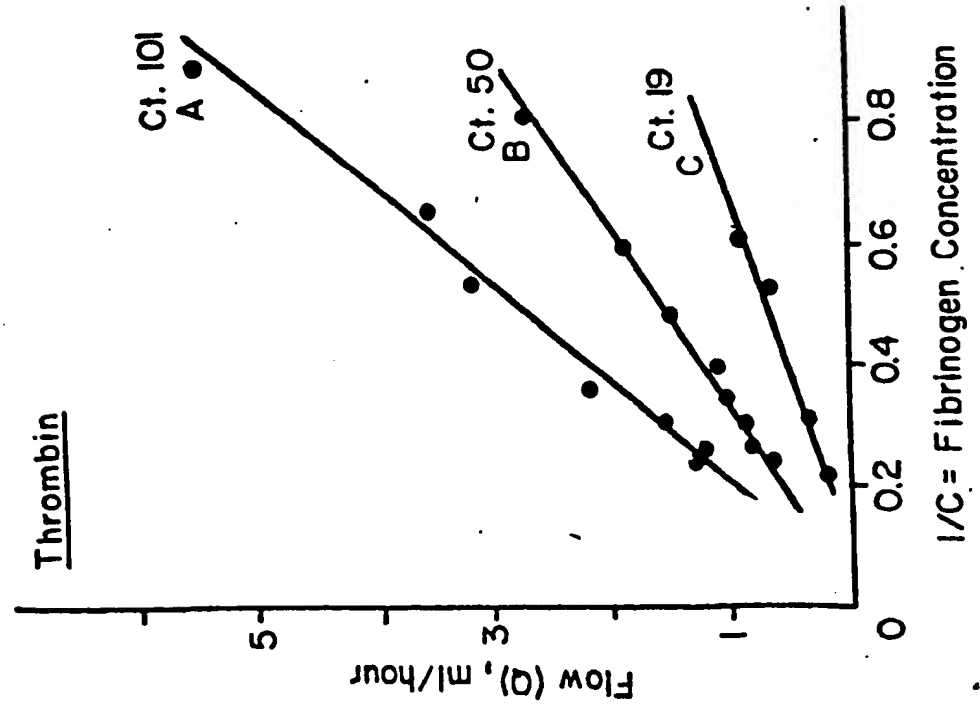


FIG. 5a.



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FIG. 6b.

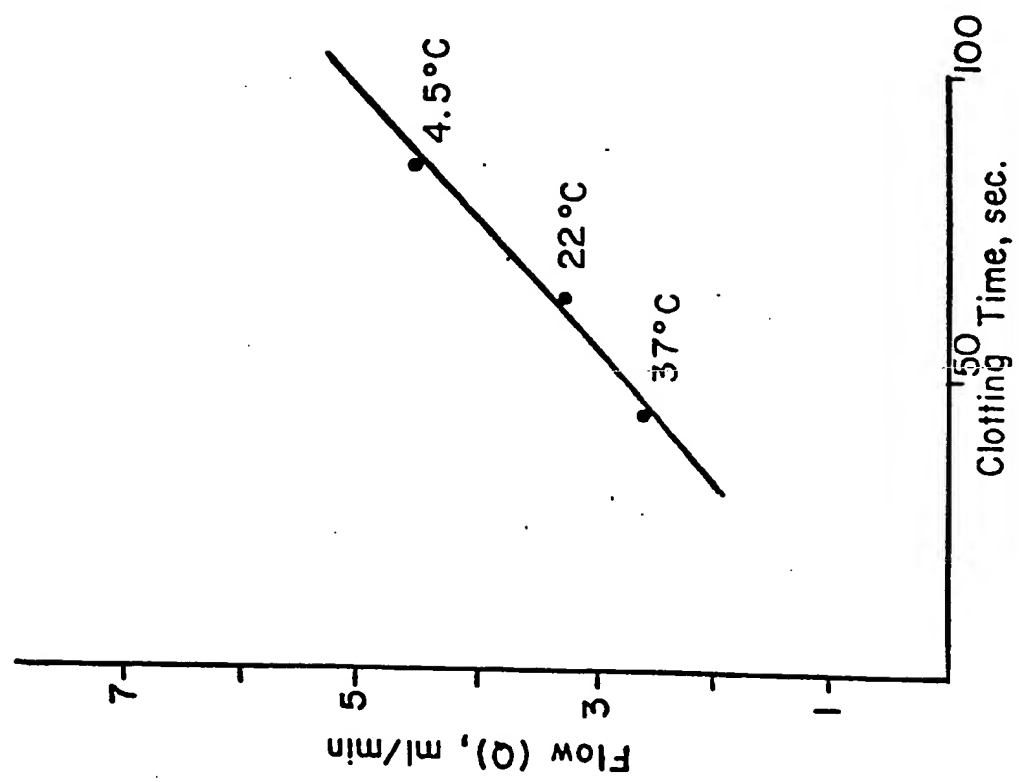


FIG. 6a.

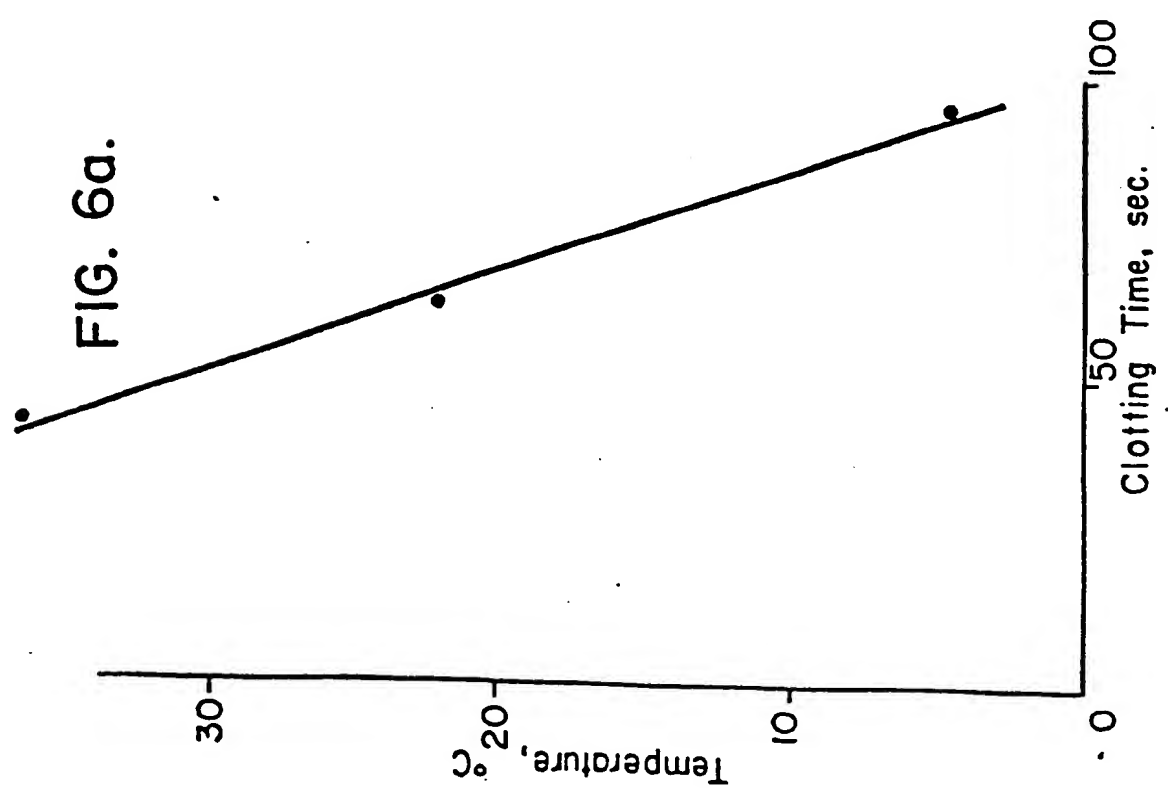
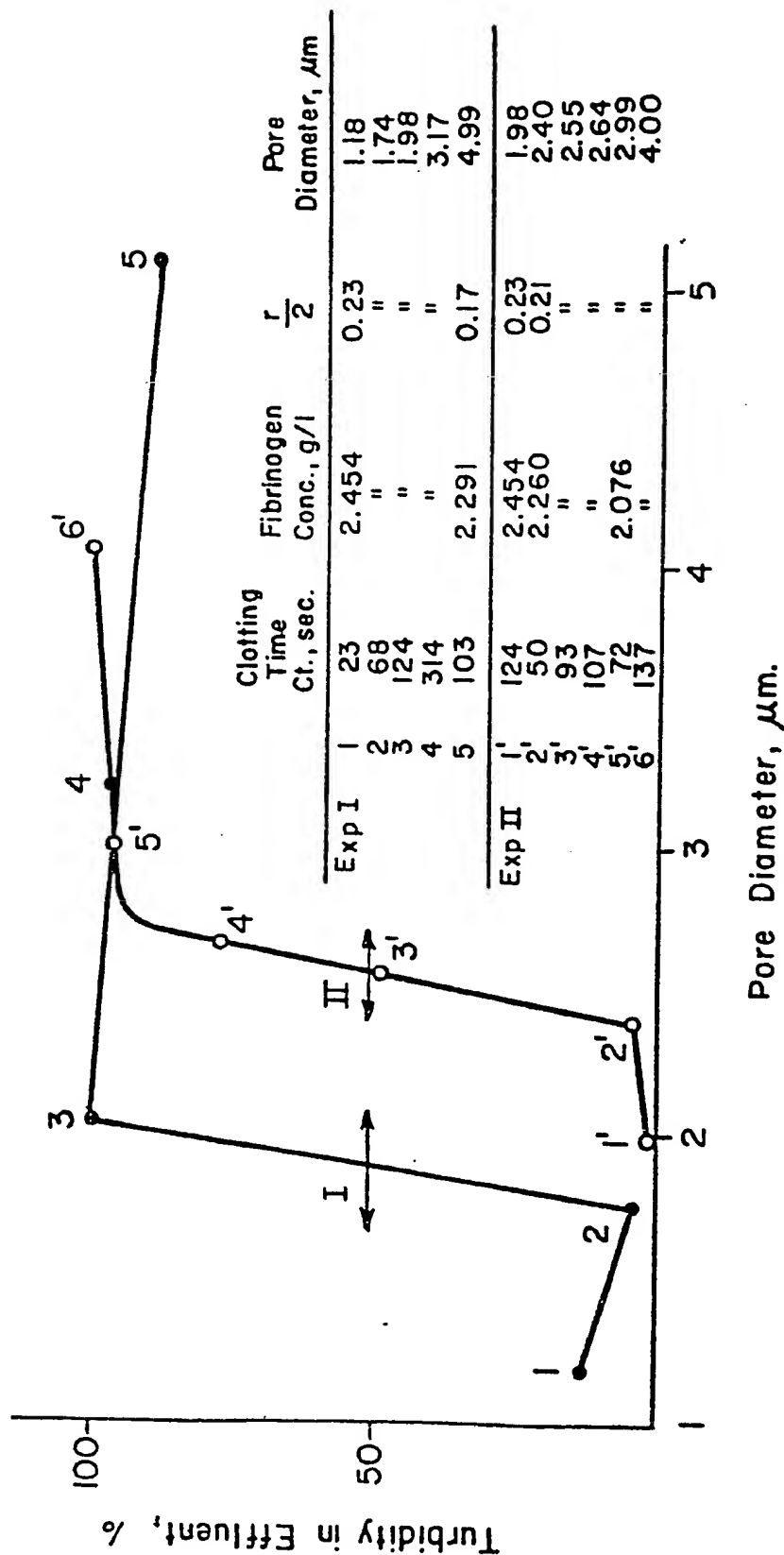


FIG. 7.





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Application number

EP 85 11 1133

Part 1

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A	DE-B-2 407 961 (W.R. VIETH et al.) * claims 1, 3, 6, 10; column 6, line 22 - column 7, line 30; examples 1-4 *	1-4, 12, 14-17	B 01 J 35/00 B 01 J 31/00 C 12 N 11/04 B 01 D 13/04
D, A	--- CHEMICAL ABSTRACTS, vol. 84, no. 9, 1st March 1976, page 227, column 1, abstract no. 55888k, Columbus, Ohio, US; Y. INADA et al.: "Fibrin membrane endowed with biological function. II. Chloroplast adenosinetriphosphatase embedded in fibrin membrane", & BIOCHEM. BIOPHYS. RES. COMMUN. 1975 67(4), 1275-1280	1, 12, 14, 15	
D, A	--- CHEMICAL ABSTRACTS, vol. 88, no. 17, 24th April 1978, page 328, column 1, abstract no. 126372h, Columbus, Ohio, US; 27-12-1977; & - A - 77 156 912 (J. SHIMITZU) --- -/-	1, 12, 14, 15	TECHNICAL FIELDS SEARCHED (Int. Cl.4) B 01 D 13/04 B 01 D 39/14 B 01 D 39/16 B 01 J 31/00 B 01 J 35/00 C 12 N 11/02 C 12 N 11/04 C 12 P 21/00 G 01 N 33/50
The present search report has been drawn up for all claims			
Place of search BERLIN		Date of completion of the search 17-02-1986	Examiner KUEHN P
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			



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Page 2

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A	<p>---</p> <p>CHEMICAL ABSTRACTS, vol. 93, no. 25, 22nd December 1980, page 376, column 1, abstract no. 234011b, Columbus, Ohio, US; Y. INADA et al.: "Fibrin membrane endowed with biological function. VI. Immobilization of multienzymes of the urea cycle", & BIOCHEM. BIOPHYS. RES. COMMUN. 1980, 96(4), 1586-1591</p>	1,12, 14,15	
A	<p>---</p> <p>CHEMICAL ABSTRACTS, vol. 92, no. 7, 18th February 1980, page 286, column 1, abstract no. 54218v, Columbus, Ohio, US; H. OKAMATO et al.: "Fibrin membrane endowed with biological function. V. Multienzyme complex of uricase, catalase, allantoinase and allantoicase", & BIOCHEM. BIOPHYS. ACTA 1980, 611(1), 35-39</p> <p>---</p> <p style="text-align: right;">-/-</p>	1,12, 14,15	
The present search report has been drawn up for all claims			
Place of search BERLIN		Date of completion of the search 17-02-1986	Examiner KUEHN P
<p>CATEGORY OF CITED DOCUMENTS</p> <p>X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document</p> <p>T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document</p>			



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A	US-A-4 261 828 (G. BRUNNER et al.) * claims 1, 3 *	1,12, 14	
A	DE-A-2 009 515 (M. PETROW) * claim *	2,3,4	
			TECHNICAL FIELDS SEARCHED (Int. Cl.4)
The present search report has been drawn up for all claims			
Place of search BERLIN		Date of completion of the search 17-02-1986	Examiner KUEHN P
CATEGORY OF CITED DOCUMENTS			
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	